# SEASONAL COMPARISON OF PREDOMINANT FACTORS IN RIVER TEMPERATURE FORMATION IN AN URBAN RIVER

Junichi Nishimata<sup>1,2)</sup>, Hitoshi Miyamoto<sup>2)</sup> (1:Nippon Koei Co., Ltd , 2:Department of Civil Engineering, Shibaura Institute of Technology)

## 1.INTRODUCTION

### • Back Ground

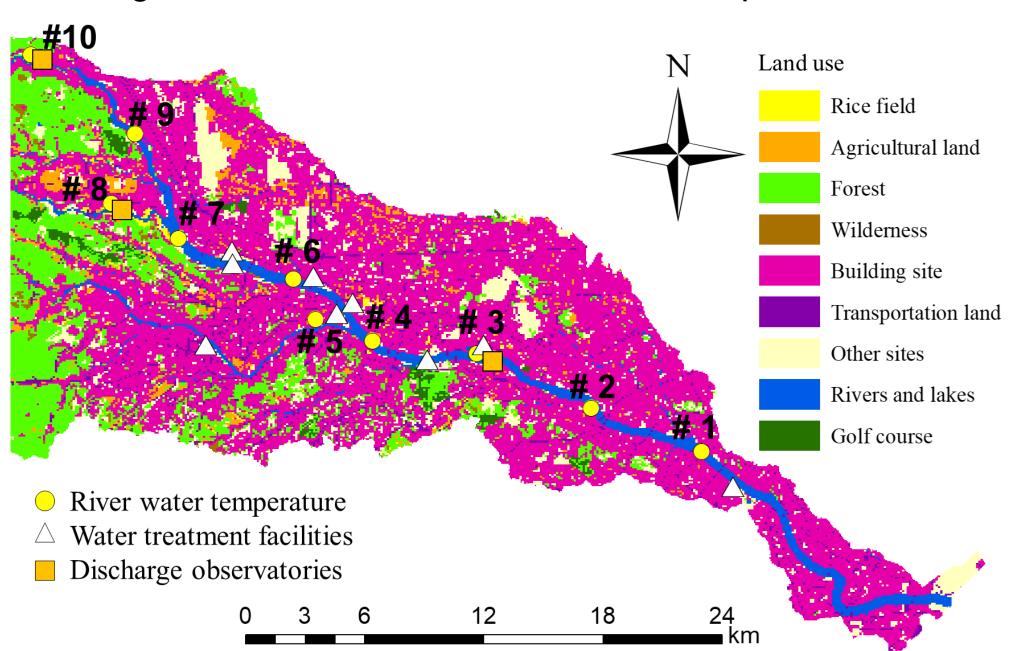
In recent years, there has been a concern that the global climate change and the artificial waste heat from urban rivers will have a significant effect on terrestrial ecosystems at river sites<sup>1,2)</sup>. River temperature is one of the important indicators that define the river environment. Purpose

The effect of the artificial waste heat of treated water on river water temperature was investigated for the Tama River. Specifically, seasonal observations of water temperature observation data are compared in the middle and downstream parts of the Tama River, and the water temperature formation factors are analyzed by using the heat transport equation.

# 2. STUDY FIELD AND RIVER WATER TEMPERATURE MONITORING

The river studied in this paper was Tama River running through the metropolitan Tokyo. Forests are predominant in the upstream part of the river basin, while, in the middle and downstream parts, the river basin has been heavily urbanized since it has been located in the metropolitan Tokyo. There are 9 water treatment facilities located along the main channel of Tama River, discharging treated sewage water with a constant water temperature of around 23 °C.

 
 Table 1. Specifications of Tama River
**River Name** Tama River 138 km Length 1240 km<sup>2</sup> Basin Area



# 3. ANALYTIC MODEL

### 3.1. Basic equation

**Basin Population** 

Basin Population density

This paper used the following one-dimensional thermal conservation equation as a basic equation of the river temperature analysis $^{3,4)}$ .

$$\frac{\partial T_w}{\partial t} = -V \frac{\partial T_w}{\partial x} + \frac{1}{C_w \rho_w h} H_{wb} + \frac{q_x}{A} (T_{wl} - T_w)$$
(1)

446 million person

3,600 person/km<sup>2</sup>

$$H_{wb} = H_s + H_a - H_{br} - H_{la} - H_{se} + H_{bed}$$
(2)

Tw: river temperature [°C], V: mean velocity [m/s], A: discharge section area [m<sup>2</sup>], Cw: specific heat at constant pressure of water[J/(kg\*K)],  $\rho w$ : water density[kg/m<sup>3</sup>], h: water depth[m], Hs: short\_wave radiation[w/m<sup>2</sup>], *Ha*: long\_wave radiation from air[w/m<sup>2</sup>], *Hbr*:long\_wave radiation from water[w/m<sup>2</sup>], *Hla*: latent heat transfer[w/m<sup>2</sup>], Hse: sensitive heat transfer[w/m<sup>2</sup>], Hbed: thermal flux from the wetted perimeter[w/m<sup>2</sup>], x: longitudinal axis, t: time[s], qx: lateral inflow in unit length[m<sup>2</sup>/s], and Twl: water temperature from the lateral inflow[°C].

### 3.2. Analytical method

The river water temperature change was estimated by using the analytical solution of Eq. (1) obtained by the method of characteristics. In this analytical solution, the river water temperature at the downstream end of the target section was calculated when the water temperature and the flow rate were given as the upstream boundary conditions. The heat fluxes on the water surface and the wetted perimeter were estimated by empirical bulk equations with the weather data from the AMeDAS system of the Japan Meteorological Agency. The water depth and the lateral inflow were determined by the least squares method of the observed and analytic temperatures with model parameters in the governing equations.

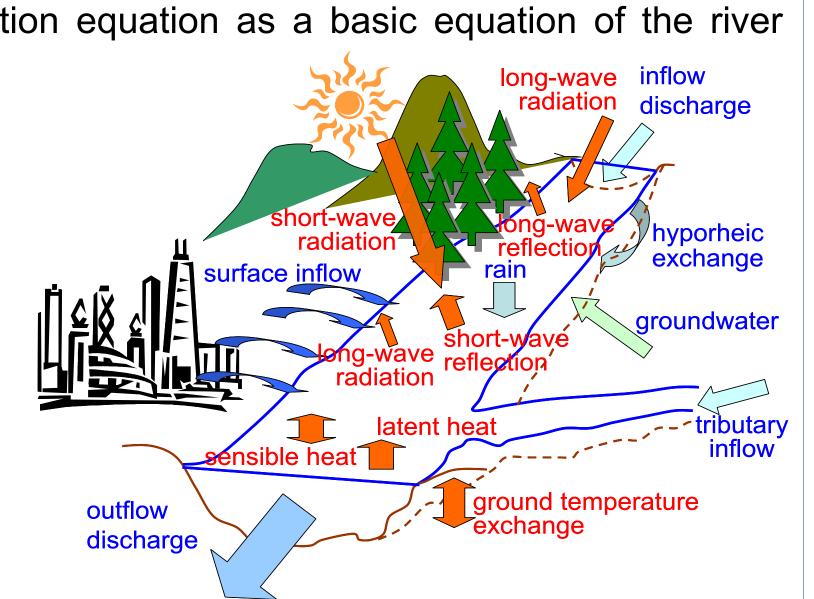
### 3.3. Point-sources treatment as a boundary condition

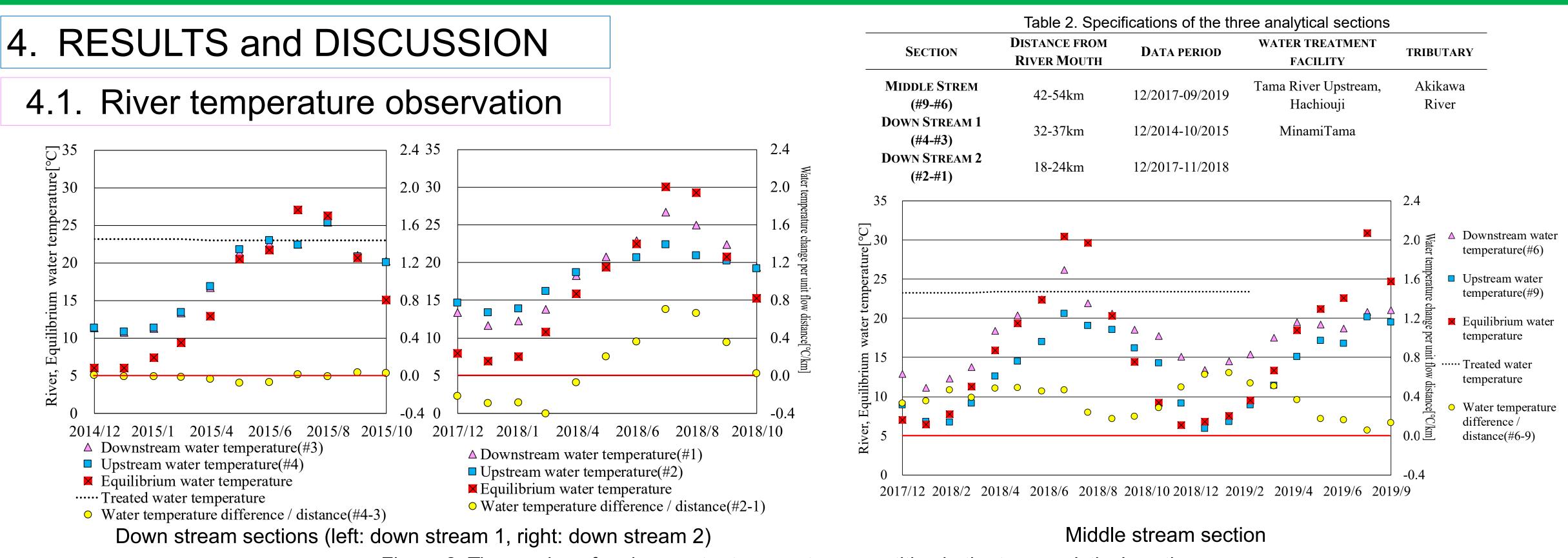
Regarding the heat inflow from treated waters and tributaries, the analytical section was divided into upper and lower sections at the inflow point, and the analytical solution was applied to each section. The conservation condition (Eq. (3)) of the heat flux before and after the division point was used as the inflow boundary condition of the divided downstream section

$$T_{wf} = \frac{Q_r T_{wr} + Q_h T_h}{Q_r + Q_h} \qquad (3)$$

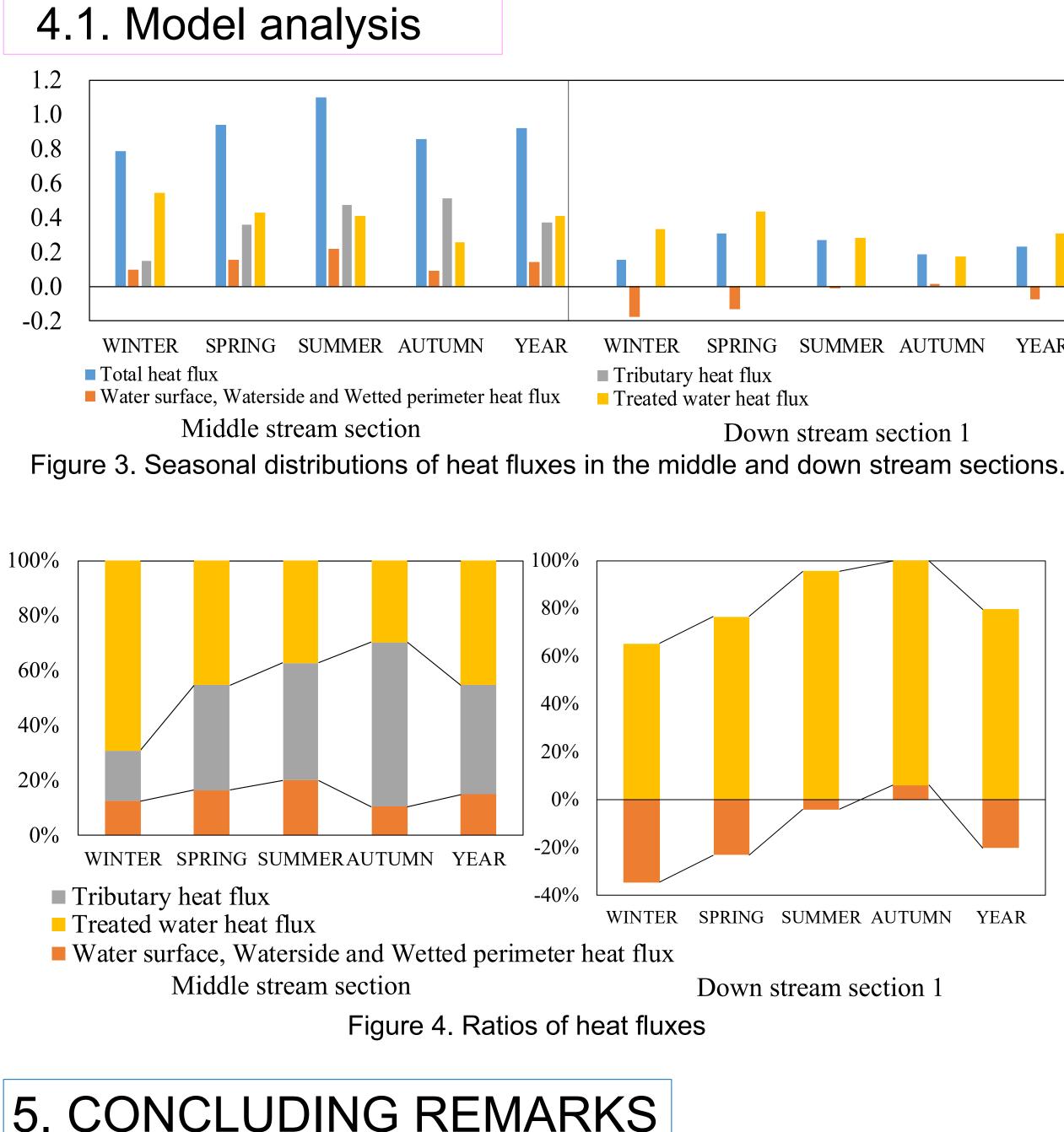
 $Q_r$ : river flow rate[m3/s],  $Q_h$ : treated water/tributary flow rate[m3/s],  $T_h$ : treated water temperature (data from the Tokyo Metropolitan Government) or tributary water temperature [°C],  $T_{wr}$ : inflow river water temperature in the main river channel at the division point [°C],  $T_{wF}$  river water temperature after the inflow [°C].

Figure 1. Tama River basin and the locations of river temperature measurements, discharge observatories and, water treatment facilities.





The (water temperature difference /distance) was quite small throughout the year in the The (water temperature difference / distance) downstream section 1. On the other hand, for the downstream section 2, positive and negative took a positive value throughout the year. In values were switched seasonally. It was considered that the formation mechanism of river water particular, its value had maximal in winter. temperature had a great influence on the presence or absence of treated water inflows. In other This could be due to the large effect of the words, it could infer that high temperature conditions were maintained continuously by the treated inflow treated water. water inflow in the down stream section 1, while the river water temperature was naturally changed due mainly to the thermal balance on the water surface in the down stream section 2.

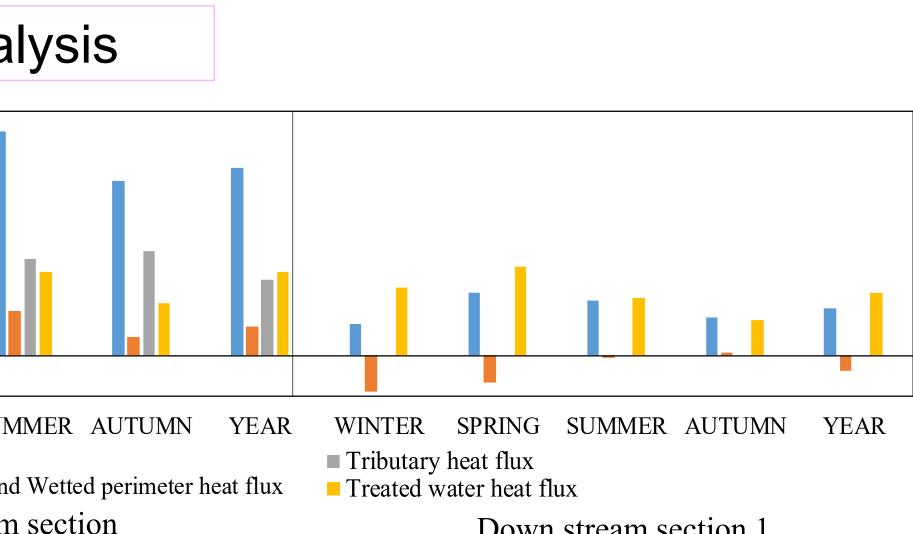


 $\cdot$  The influence of the treated water inflow extended to the entire river course of the Tama River. • In particular, it revealed that the influence became larger in the middle stream section than in the down stream sections, and most predominant in winter.

References

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Figure 2. Time series of various water temperature quantities in the tree analytical sections



The values of the fluxes in Fig. 3 were devided by unit downstream distance. In Fig. 3, the values during the period of fine weather were collected and calculated for discussion. It was revealed from Fig. 3 that the total heat flux was larger in the middle section than that in the downstream section 1. It corresponded to the characteristics found in the (water temperature difference / distance) relationship in Fig. 2. The heat flux of the treated water in winter was the largest in the middle section, while that in spring was the largest in the down stream section 1. It could suggest that the season in which the effect of treated water was predominant differed largely in each section. Furthermore, it also indicated in Fig. 3 that the heat flux of the water surface, wetted perimeter, and lateral inflow had negative or nearly zero in summer and autumn in the down stream section, meaning that the treated water inflow was only contributed to the temperature formation.

Figure 4 showed the ratios of each heat flux in the middle stream section and the down stream section 1. In the middle stream section, the effect of treated water on the river water temperature became most predominant in winter, and its ratio was reached to 70%. This result was also confirmed in the water temperature analysis in Fig. 2. On the other hand, in the down stream section 1, the model analysis revealed that the formation mechanism of the river water temperature was completely different in each season, though the river temperature change was quite small as shown in Fig. 2 (b). Namely, in winter and spring, the river water temperature was kept constant by the balance between a warming effect of the treated water and a cooling effect of the heat fluxes from the water surface, wetted perimeter, and lateral inflow.