IMPROVEMENT OF THE MIXING LENGTH MODEL AND NUMERICAL CALCULATION OF THE FLOW OVER A BACKWARD-FACING STEP

INTRODUCTION

In this paper, based on the comparative study of the two models, an improved mixed turbulence model is firstly proposed by means of dimensional analysis, in which the calculation formula of eddy viscosity coefficient includes not only 2.5 **H** 2 Re=4800 profile x/h=1 Comparison of Velocity Distribution turbulent kinetic energy k and its dissipation rate ε , but also the velocity gradient of the mean field. Then the model is Experimental Value applied to the numerical simulation of the flow over a backward-Model mproved Mixed Turbulence Model facing step. And the calculated longitudinal velocity profile, turbulent kinetic energy k and dissipation rate ε distribution 0.5 of separation zone are analyzed. Meanwhile, by comparing with some measured data and the calculation results under the -0.5 standard $k-\epsilon$ model, it is fortunately found that in the range of Reynolds number (Re) from $5 \times 10^3 - 1 \times 10^5$, the improved mixed 0.2 0.4 turbulence model with velocity gradient can predict this type of turbulent flow more accurately. 2.5 ۲h Re=50000 profile x/h=1 Comparison of Velocity Distribution **IMPROVED MIXED TURBULENCE MODEL** k-£ Model Improved Mixed Turbulence Model +P0.8 0.6 Turbulent Eddy Viscosity Coefficient (Obtained by Dimensional Analysis) Figure 2. Longitudinal velocity distribution of x/h=1 section CALCULATION AREA >2 Re=4800 Profile x=h Comparison of Turbulence Kinetic Energy Improved Mixed Turbulence Model — k-ε Model → FLOW INLET OUTLET Backflow Region -0.5 11111111111111111111111 1200 1 5.0E-04 1.0E-03 k/(m2/s2) Figure 1. Schematic diagram of calculation area (unit: mm)

k	Equation
3	Equation

$\frac{\partial k}{\partial t}$	$+ \overline{u}_{l} \frac{\partial k}{\partial x_{l}} = \frac{\partial}{\partial x_{l}} \left(C_{k} \frac{k^{2}}{\varepsilon} \frac{\partial k}{\partial x_{l}} \right) -$	- E
$\frac{\partial \varepsilon}{\partial t}$	$-\overline{u}_{l}\frac{\partial\varepsilon}{\partial x_{l}} = \frac{\partial}{\partial x_{l}}\left(C_{\varepsilon}\frac{k^{2}}{\varepsilon}\frac{\partial\varepsilon}{\partial x_{l}}\right) + C_{\varepsilon^{1}}\frac{\varepsilon}{k}$	<i>P</i> -

$$v_t = f(k, \varepsilon, \frac{du}{dy}) = C \frac{k^3}{\varepsilon^2} \left| \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right| = C_{\mu} \frac{k^2}{\varepsilon}$$



CONCLUSION

For the uncertainty of the mixed length | in complex flow, we consider expressing | as a function of the turbulent kinetic energy k and its dissipation rate ε. And an improved mixed turbulence model considering the turbulent kinetic energy k, dissipation rate ε and mean field velocity gradient is proposed. rulate the improved mixed turbulence model can not only better simulate the wall under the condition of large Reynolds number, but also successfully simulate the additional separation vortex downstream the main separation zone. r the improved model can better simulate the distribution of kinetic energy dissipation rate ε.

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Figure 4. Distribution of turbulent kinetic energy and turbulent kinetic energy dissipation rate at the profile x/h=1.



ANALYSIS AND **COMPARISON OF** CALCULATION RESULTS

The improved model can obtain the velocity profile closer to the experimental data as figure 2 shows.

The improved model can successfully simulate this separated-flow region as figure 3 shows.

The improved model is superior in the simulation of the turbulent kinetic energy near the boundary, and can credibly calculated the the turbulent kinetic energy dissipation rate as figure 4 shows.